

The Study of the Strength Properties of Galvanized Iron (GI) Fiber Reinforced Concrete

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ABSTRACT The use of concrete with randomly distributed metallic or non-metallic fiber is now prominent in concrete engineering and metallic fiber has been reported to have a better contribution to concrete mechanical properties. The utilization of locally available galvanized iron or metallic fiber as a bridging material which is a new technique in Bangladesh has the ability to surprisingly improve concrete physical properties. This research was, therefore, conducted to compare the concrete performance of GI fiber and steel fiber using previous literature as well as the suitability of GI fiber as a supplant to steel fiber in the concrete industry. This was achieved through the evaluation of the compression, tension, and brittleness of concrete with 'Galvanized Iron' fiber using several cutting lengths of 20 mm and 40 mm with multiple mix proportions including 1.0%, 1.5%, 2.0%, and 2.5% by volume of the concrete. The results showed the fiber with a large cut length of 40 mm and proportion lesser than 2.5% performed well than 20 mm with proportion >2% in reference to the plain concrete. Moreover, the incorporation of a 2.0% proportion of galvanized iron fiber with 40 mm length was observed to have exhibited crowning increment for both concrete compression and tension by 16.1% and 89.2% correspondingly contrasted to the control specimen. A further increase in the percent of fiber content >2% led to a reduction in the compression and tension for both 20 mm and 40 mm lengths while a significant reduction in brittleness for galvanized iron fiber reinforced concrete was observed in contrast to the control specimen. Furthermore, the inclusion of 1.0%–2.5% GI fiber with a 40 mm length reduced concrete brittleness by 56.9% - 65.5 % in comparison with the control specimen. Therefore, the inclusion of galvanized iron (metallic) to enhance the physical properties of concrete was deduced to be one of the startling stratagems.

KEYWORDS Metallic Fiber Reinforced Concrete; Galvanized Iron (GI); Compression; Tension; Brittleness.

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1 INTRODUCTION

Building construction materials such as concrete which is produced through a carefully proportioned mixture of cement, sand, gravel or other aggregates, and water and hardened in different forms and dimensions for the specified structure. The materials are amalgamated to ensure the voids within the aggregates are satiated to produce a consistent dense concrete. It is important to note that concrete has been the foremost widely used construction material throughout the planet with those made using hydraulic cement observed to be having certain characteristics while plain and unreinforced concrete is a friable material with a picayune strain capacity (Islam, G. M. S, et al., 2016). Concrete is relatively sturdy in compression but languid in tension and tends to be fragile. This,

therefore, makes it important from the engineering perspective and there has been a continuing effort to upgrade its performance.

The greatest abridgment for concrete is the lack of ductility and the improvement of this aspect is a prime concern for civil engineers. This has, therefore, led to a considerable number of studies incorporating different fibers such as steel, jute, glass, and polymer in concrete (Nemati, K. M, 2013). The concept is generally known as the Fiber Reinforced Concrete (FRC) and has been found to be one of the foremost promising new construction materials due to its enhanced ductility and decreased brittleness (Rouhi, J, et al., 2011). The inclusion of the fibers also modifies the behavior of the fiber-matrix

composite after it has cracked, thereby, upgrading its toughness.

The real contribution of the fibers is to extend the toughness of the concrete (Sivakumar. A, et al., 2007) which has been described to be an area under a load-deflection curve. This is due to the fact that plain concretes fail suddenly once the greatest strength is surpassed while fiber ferroconcrete continues under considerable loads even at deflections considered more than the fracture deflection in plain concrete. This means fiber-reinforced concrete is in a position to sustain load or strain much greater than plain concrete (Kim, J. S, et al., 2017).

Fiber ferroconcrete is also generally defined as a material made with hydraulic cement, aggregate, and incorporating discrete discontinuous fiber (ACI 544.4R-88, 1999). Galvanized steel wire or iron (GI) formed from zinc-plated steel is presently used as a reinforcement to improve concrete properties mainly due to the ability of the protective layer of zinc to inhibit corrosion. Several studies have been conducted to investigate the suitability of GI fibers as an alternative to steel or hybrid fibers. This is important considering the fact that steel fiber is the most prominent metallic fiber with the ability to augment concrete properties but it is expensive to be used in Bangladesh due to additional cost attached to its unavailability in the local market. Studies have also been conducted to determine the substitute reinforcing material to emulate steel fiber in improving the mechanical properties of concrete at a lower cost. Some others also focused on using different mix proportions of steel fiber to determine their effectiveness but there is no significant research on the use of GI fiber with different cutting length and at several mix proportions.

This means it is considerably important to determine the influence of the effective

utilization of galvanized iron (GI) fiber to produce ennobled concrete. Therefore, the foremost objective of the study was to develop galvanized iron (GI) fiber reinforce concrete composites, and determine the suitable length and content (volume fraction) of fibers based on concrete mechanical behavior.

2 MATERIALS AND METHODS

2.1 Portland Cement

Ordinary hydraulic Cement containing 95–100% and 0–5% of clinker and gypsum respectively at a precise gravity of 3.12 was used in this study.

2.2 Coarse and Fine Aggregates

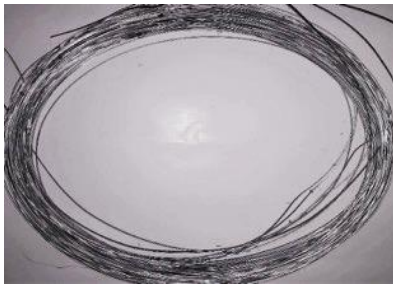
Sylhet sand was utilized as the fine aggregate while crushed stone chips were treated as the coarse aggregate using a grading consistent with ASTM C33. The aggregates were collected from Sylhet and their physical properties are presented in Table 1.

Table 1. Physical characteristics of aggregates

Property	Sand	Stone Chips
Bulk Specific Gravity (OD Basis)	2.54	2.66
Absorption Capacity (%)	1.34	0.69
Fineness Modulus (FM)	2.62	-
Dry Rodded Unit Weight (kg/m ³)	1590	1550

2.3 Galvanized Iron Fiber

Galvanized iron (GI) fiber has a circular section with the diameters varying from 0.37 mm to 5 mm but those with 1mm diameter were used in this study. According to the manufacturers, the materials are resistant to high temperature and corrosion and also provide high strength considering the properties shown in Table 2. Two different cut lengths including 20 and 40 mm as presented in Fig. 2 were used in this study at different volumetric percentages of 1%, 1.5%, 2%, and 2.5% in the concrete mixture.



(a)



(b)



(c)

Figure 1. (a) Galvanized iron (GI) (b) GI with 20 mm length (c) GI with 40 mm length

Table 2. Characteristics of Galvanized iron (GI) fiber employed in this study (American Galvanizers Association)

GI Fiber	Feature
Cutting Length (mm)	20
Cutting Length (mm)	40
Diameter (mm)	1
Aspect Ratio (l/d)	20
Aspect Ratio (l/d)	40
Density (kg/m ³)	6000
Tensile Strength (MPa)	250
Color	Silver
Elastic Modulus (GPa)	6.0

2.4 Concrete Mix Proportions

Trial mixtures were prepared to obtain the targeted strength of 35 MPa at 28 days with a target slump value of 75–100 mm. The concrete mix was designed according to the standards of the American Concrete Institute (ACI 211, 2009). The fibers added reduced the slump value due to the interweaved arrangement of fibers in the concrete matrix. Therefore, additional water was needed compare to control concrete to keep the slump within the mix design range. The detailed mix proportions of the constituent materials, with the SSD condition where applicable, to produce the concretes used in this study are presented in Table 3.

2.5 Concrete Mixing, Casting, and Curing

The concrete mixture was prepared with different parameters including the length and volume fraction of the iron fiber content while the cut lengths of the fiber were 20 and 40 mm at 1%, 1.5%, 2%, and 2.5% proportion. The fibers were truncated to the desired length using a wire cutting machine while the concrete was prepared through a machine mixer by considering a 50-liter volume for each trial blend. The process involved mixing the appropriate quantity of coarse aggregates, fine aggregates, and cement followed by the inclusion of the iron fibers to obtain congruous distribution in every part of the concrete after which water was added with four minutes of vigorous mixing to achieve consistency. A slump cone was used to measure the workability of the mixture while a 150 mm cube specimen was set and placed in a circumambient temperature for 24 hours to conduct laboratory strength tests. Subsequently, the specimens were extracted from the mold and placed in a curing tank to determine the strength at 7 and 28 days.

Table 3. Mixing composition of concrete utilized in laboratory works (Galvanized iron)

Proportion	Water (kg/m ³)	Cement (kg/m ³)	CA (kg/m ³) [SSD]	FA (kg/m ³) [SSD]	GI (kg/m ³)
Control Concrete GIF0(0.0%)	215	566	999	565	0.0
Galvanized Iron (20 mm)					
GIF1 (1.0%)	218	566	999	565	23.45
GIF2 (1.5%)	219	566	999	565	35.17
GIF3 (2.0%)	223	566	999	565	46.90
GIF4 (2.5%)	225	566	999	565	58.63
Galvanized Iron (40 mm)					
GIF5 (1.0%)	217	566	999	565	23.45
GIF6 (1.5%)	220	566	999	565	35.17
GIF7 (2.0%)	223	566	999	565	46.90
GIF8 (2.5%)	224	566	999	565	58.63

2.6 Compression Test

The compression of the concrete was tested using EN 12390-3 (2009). The compressive strength has been considered the most prominent feature of concrete compared to other physical properties due to its structural significance and the provision of a limpid repercussion on how the increment of fiber proportions influence the concrete strength. Moreover, the load was implemented with a strain rate of 1.5mm/min up to the period the specimens reached their fracture point. The highest load received by the concrete specimen throughout the test was inscribed. The experimental set up is, therefore, shown in the following Figure 2.

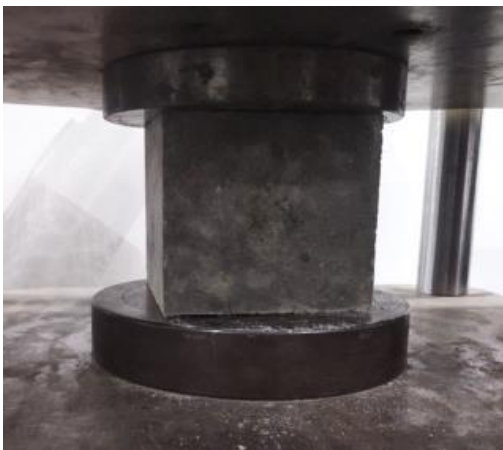


Figure 2. Laboratory arrangement for compression test.

2.7 Tensile Strength Testing

The friableness and modicum tensile strength of concrete make it callow to flounder with the direct tension. Therefore, assessing concrete tension is imperative to ascertain the load required for fracture through the use of a splitting experiment in accordance with the EN 12390-6 (2000). The tensile strength was, however, measured using Equation (1)

$$f_{ct} = 2F/\pi Ld \quad (1)$$

where f_{ct} is the tensile strength in N/mm², F is the maximum load in Newtons (N), L is the length of the specimen in millimeters (mm), and d is the size of a designated cross-section in millimeters (mm).

3 RESULT AND DISCUSSION

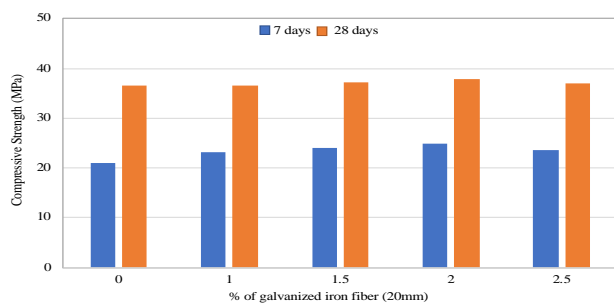
3.1 Compressive Strength

Compressive strength is the most fundamental property of concrete due to its main function of withstanding compressive stress. The behavior of concrete under compression load due to the utilization of galvanized Iron metallic fiber is presented in Figures 3 and 4. Meanwhile, the results presented in Table 4 showed the integration of galvanized iron fiber in concrete enhanced the compressive strength.

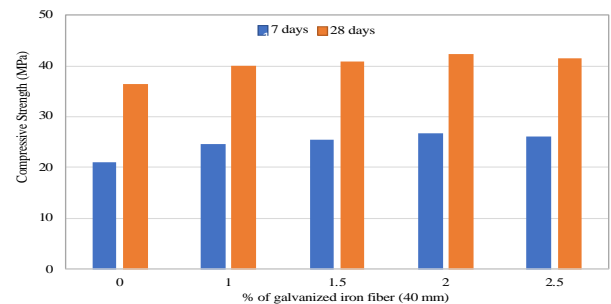
Table 4. Experimental outcomes of concrete compression

Length (mm)	Concrete Composition	Compressive strength at 7 days (MPa)	Compressive strength at 28 days (mpa)	28 days strength increment (%)	Steel Fiber*	Compressive strength at 28 days (MPa)*
20	Control concrete	21.023	36.5	-	0	33.4
	GIF1	23.12	36.58	0.2	0.5%	37.83
	GIF2	24.06	37.24	1.8	1.0%	43.74
	GIF3	24.83	37.79	3.5	1.5%	48.03
40	GIF4	23.64	36.91	1.1	-	-
	GIF5	24.70	39.92	9.3	-	-
	GIF6	25.43	40.86	11.9	-	-
	GIF7	26.67	42.35	16.1	-	-
	GIF8	26.13	41.52	13.8	-	-

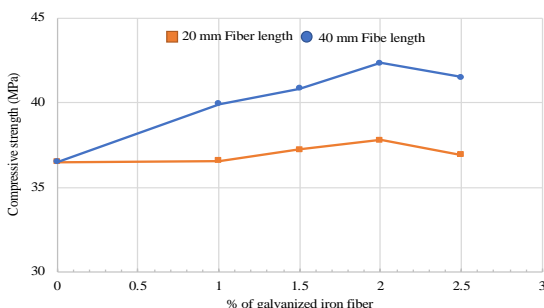
* Joshi A, et.al; 2016



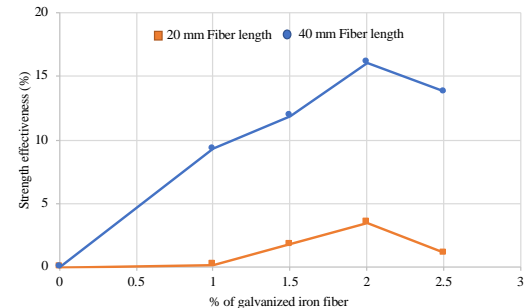
(a)



(b)



(c)



(d)

Figure 3. Change in the compressive strength of concrete at different fiber proportions (a) 20 mm length of Galvanized Iron (b) 40 mm length of Galvanized Iron (c) the comparison between compression for 20 mm and 40 mm length (d) comparison between the strength improvement between 20 mm and 40 mm length.



(a)



(b)

Figure 4. Concrete cube after compression test (a) Control specimen (b) GIF (1.5%).

Figures 3a and 3b compare the compressive strengths on the 7th and 28th day for 20 mm and 40 mm fibers respectively and the values were observed to have aggravated up to 2% GI fiber and later reduced as the proportion increased. This was associated with the confining effect of fibers in the concrete matrix which holds the materials together. Meanwhile, this effect depends mainly on the difficulty in controlling the orientation of fibers due to its random distribution in the concrete matrix. Figure 4, however, shows the holding capacity of GI fiber to be lucid with the increment in the strength of the reinforced concrete found in the range of 0.2 % to 3.5% for 20 mm length and 9.3% to 16.1% for 40 mm. A slight decrease was observed in the two specimens for 2.5% proportion and this is associated with the high dosage of fiber which affects the concrete's cohesiveness. The best result was, however, recorded at 2% proportion with 40 mm length as observed with the 16.1% increment in the compressive strength of the concrete. This is in agreement with the findings of previous research by Joshi et al [16] that it is possible to increase the compressive

strength of concrete within a range of 13.8% to 43.8% by incorporating steel fibers.

3.2 Tensile Strength

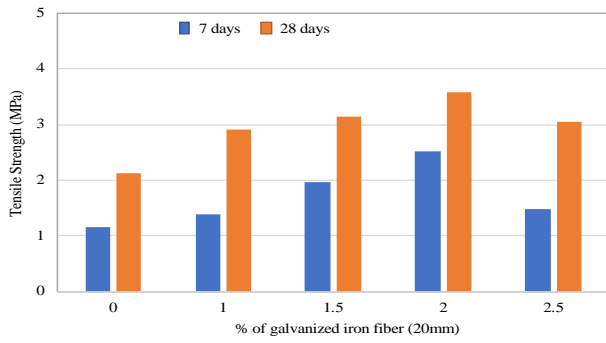
Split tensile strength is the ability of concrete to withstand tension with the effect of the GI fiber incorporated determined using a split tensile test and the results obtained are presented in Table 5 and the changes recorded are demonstrated in Figure 5.

The incorporation of GI fibers was observed to have increased the split tensile strength of the reinforced concrete compared to the control specimen. Figure 5(d) represents the effectiveness of the splitting tensile strength for the specimens at 28 days with the galvanized Iron fiber reinforced concrete observed to have increased significantly compared to the plain concrete. Moreover, the splitting tensile strength of the reinforced concrete was found to have increased in a range of 36.6% to 67.6% for 20 mm length as the fiber content increased while 40 mm length was observed to have shown a better performance with 70% to 89.2%.

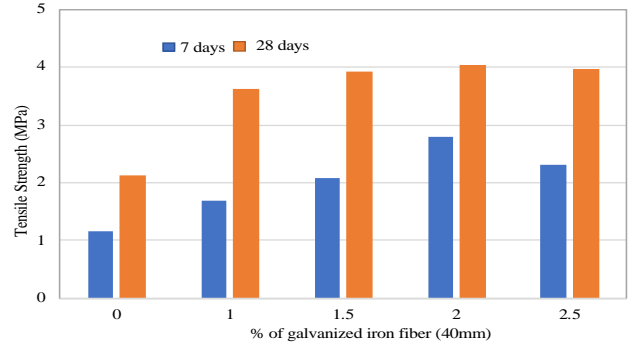
Table 5. Experimental outcomes of concrete compression

Length (mm)	Concrete Composition	Tensile Splitting Strength at 7 Days (MPa)	Tensile Splitting Strength at 28 days (MPa)	28 days Strength Increment (%)	Steel Fiber*	Tensile splitting Strength at 28 days (MPa)*
-	Control Concrete	1.17	2.13	-	0	2.67
20	GIF1	1.39	2.91	36.6	0.5%	3.34
	GIF2	1.97	3.13	46.9	1.0%	3.83
	GIF3	2.52	3.57	67.6	1.5%	4.62
	GIF4	1.49	3.04	42.7	-	-
40	GIF5	1.70	3.62	70	-	-
	GIF6	2.09	3.93	84.5	-	-
	GIF7	2.79	4.03	89.2	-	-
	GIF8	2.32	3.97	86.4	-	-

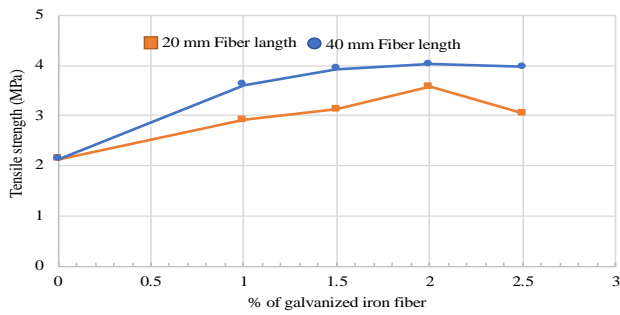
* Joshi A, *et.al*; 2016



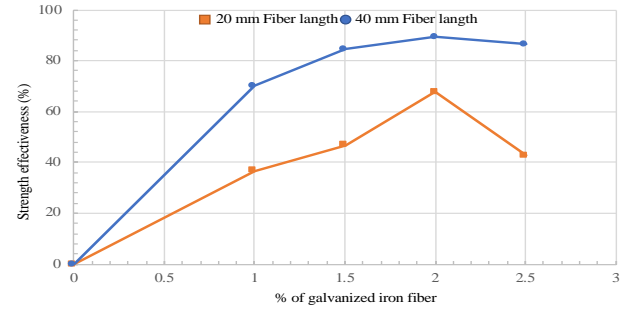
(a)



(b)



(c)



(d)

Figure 5. Change in concrete tension due to the fiber proportion in (a) 20 mm length (b) 40 mm length (c) comparison in the tension between 20 mm and 40 mm length (d) comparison with the strength increment between 20 mm and 40 mm length.



(a)



(b)

Figure 6. Concrete cube after the tension test (a) control Specimen (b) 1.5% GIF.

The most effective result indicated by an 89.2% increment in the tension was found with a 2% mix proportion for 40 mm length. This means a lengthy fiber with averagely $\leq 2\%$ of GI leads to the production of a concrete mixture which is able to withstand cracking under a tensile load as shown in Figure 6. Meanwhile, more proportion of GI fiber which is $>2\%$ were found to have produced an incongruous mixture due to

the deficiency caused by the free rearrangements of the concrete elements. The incorporation of 2.5% GI fiber was, however, discovered to have provided a superior contribution to tensile strength than the control specimen. Moreover, the previous research by Joshi et al [16] showed the possibility of enhancing concrete tension by adding steel fiber. This further confirms the ability of GI fiber to

produce analogous effects when added to the concrete even though the increment of strength is a bit higher for SFRC.

3.3 Influence of galvanized Iron fiber on concrete brittleness

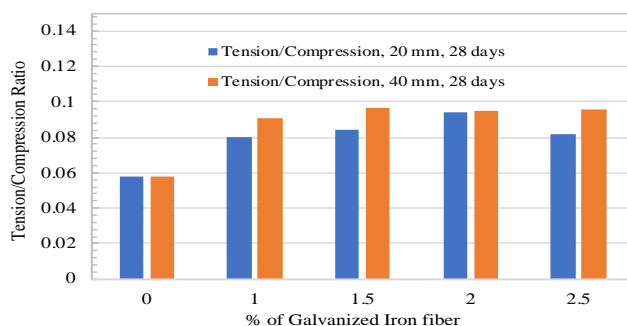
Concrete with high strength exhibits high friableness and this makes it important to appraise concrete performance, especially by using the ratio of tension to compression to determine its fragility (Li W, *et.al.* 2014 and Li. R, *et.al.* 2014) such that a higher ratio leads to lesser frailty. The results of the concrete brittleness due to the addition of galvanized iron are presented in Table 6 while the comparison based on the lengths is shown in Figure 7.

The most luminous difference between GI fiber-reinforced and plain concretes is the characteristics of the failure. Figure 6 conspicuously shows brittle failure in the plain

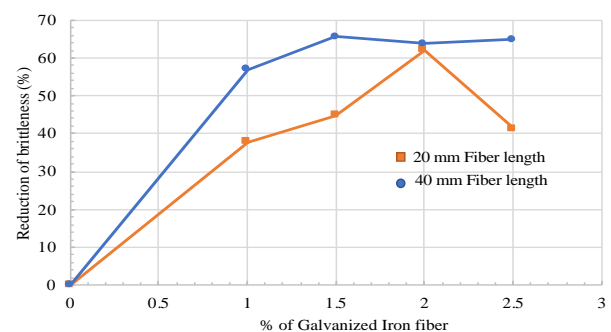
concrete as observed in it splitting into two pieces while ductile failure was found with GI fiber reinforced concrete which prevents it from splitting. Moreover, the fibers were also found to have aligned with the direction of the tension such that an increase in their proportion leads to a stable enhancement in the ratio of tension to compression. The use of galvanized iron fiber also reduced the frailty as observed with the 37.9% to 62.1% recorded for 20 mm length and 56.9% to 65.5% for 40 mm length compared to the control specimen. Furthermore, the GI fibers immerse the crack by reinforcing the concrete whenever a fracture is originated. Those with high lengths were discovered to influence proper distribution due to their large specific area which increases the mechanical entanglement in the concrete. It is also important to note that the addition of a GIF with a 40 aspect ratio is much better to suppress brittleness than the 20 aspect ratio.

Table 6. Experimental outcomes of concrete brittleness

Type of Concrete	Fiber Content (%)	Tensile to Compression Ratio	Reduction of Brittleness of Concrete (%)
Control Concrete	0	0.058	-
GIF1	1.0	0.080	37.9
GIF2	1.5	0.084	44.8
GIF3	2.0	0.094	62.1
GIF4	2.5	0.082	41.3
GIF5	1.0	0.091	56.9
GIF6	1.5	0.0962	65.5
GIF7	2.0	0.095	63.7
GIF8	2.5	0.0956	64.8



(a)



(b)

Figure 7. Change of concrete tensile/compression ratio with GI fiber proportion (a) Showing disparity of concrete brittleness between 20 mm and 40 mm length of galvanized iron (b) Showing disparity of concrete attenuation of brittleness between 20 mm and 40 mm length of galvanized iron.

4 CONCLUSION

Laboratory experiments were conducted to determine the compression, tension, and brittleness of the concretes reinforced with 'Galvanized Iron' fiber. The results showed 20 mm length galvanized iron fiber was able to aggravate concrete compressive strength by 0.2 % - 3.5%, increased tension by 36.6% - 67.6%, and reduced brittleness by 37.9% - 62.1 % while 40 mm length had 9.3% - 16.1%, 70% - 89.2%, and 56.9% - 65.5 % respectively. The use of a 40 mm length for 2% GI fiber proportion was found to be the best mixture as observed in its effect on the compression with a 16.1% increase, tension with 89.2% increase, and brittleness with 63.7% crack reduction.

In comparison with steel fiber, the utilization of GI fiber showed a bit smaller enhancement in concrete compression and tension and has the potential to be used as a substitute for the expensive imported steel fiber in Bangladesh. This is due to the local availability of the GI fiber in the country which makes it a viable low-cost substitute in fiber reinforced concrete and its ability to improve the mechanical properties of concrete, especially the tension and brittleness.

DISCLAIMER

The authors declare no conflict of interest.

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REFERENCES

ACI 211.1, 2009. *Standard Practice for Selecting Proportions for Normal, Heavyweight and Mass Concrete*. American Concrete Institute, Farmington Hills, MI, 48331-3439, USA.

ACI 224.1R, 2007. *Causes, Evaluation, and Repair of Cracks in Concrete Structures*. American Concrete Institute, Farmington Hills, MI, 48331-3439, USA.

American Galvanizers Association. *ASTM Specifications*. [Online] Available at: <https://galvanizeit.org/specification-and-inspection/coating-specifications/astm-specs#ASTMmainstandards> [Accessed 12 September 2019].

Darole, E. R. J. S., Kulkarni, V.P., Shaikh, A.P. and Gite, B.E., 2013. Effect of Hybrid Fiber on Mechanical Properties of Concrete. *International Journal of Engineering Research and Applications (IJERA)*, 3, pp.1408-1411.

EN 12390-03, 2009. Testing Hardened Concrete, Part-3: Compressive Strength Test of Concrete. *European Committee for Standardization*, Avenue Marnix 17, B-1000 Brussels, Belgium.

EN 12390-06, 2000. Testing Hardened Concrete, Part-6: Tensile Splitting Test of Concrete. *European Committee for Standardization*, Avenue Marnix 17, B-1000 Brussels, Belgium.

Islam, G. M. S. and Gupta, S. D., 2016. Evaluating Plastic Shrinkage and Permeability of Polypropylene Fiber Reinforced Concrete. *International Journal of Sustainable Built Environment, Elsevier*, 5, pp.345–354.

Joshi A., Reddy, P, Kumar, P. and Hatker, P. 2016. Experimental Work on Steel Fibre Reinforced Concrete. *International Journal of Scientific & Engineering Research (IJSER)*, 7, pp.971-981.

Kim, J. S., Cho, C. G., Moon, H. J., Kim, H., Lee, S. J. and Kim, W., 2017. Experiments on Tensile and Shear Characteristics of Amorphous Micro Steel (AMS) Fibre-Reinforced Cementitious Composites. *International Journal of Concrete Structures and Materials*, 11, pp.647–655.

Li, R., Zhang, X. H. and Meng, Y. F., 2014. Study of Performance on Reduce Fragility and Increase the Toughness of Fly Ash Ceramsite Concrete. *Advanced Materials Research*, 997, pp.120-123.

Li, W., Huang, Z. and Wang, X. C., 2014. Study on Tension and Compression Ratio and Discount Ratio of Rubber Modified Silica Fume Concrete. *Applied Mechanics and Materials*, 670-671, pp. 396–400.

Nemati, K. M., 2013. Fiber Reinforced Concrete (FRC). *Concrete Technology*, University of Washington.

Rouhi, J., Jamshidi, M. and Kakooei, S., 2011. The Effects of Polypropylene Fibers on the Properties of Reinforced Concrete Structures. *Construction and Building Materials*, 27, pp.2586-2481.

Sivakamasundari, S. and Balamurugan, S., 2019. Mechanical Properties of Hybrid Fiber Concrete. *International Journal of innovative Technology and Exploring Engineering (IJITEE)*, 8, pp.146-150.

Sivakumar, A. and Santhanam, M., 2007. A Quantitative Study on the Plastic Shrinkage Cracking in High Strength Hybrid Fibre Reinforced Concrete. *Cement Concrete Composite*, 29, pp.575–581.

Vairagade, S. V. and Kene, S. K., 2013. Strength of Normal Concrete Using Metallic and Synthetic Fibers. *Procedia Engineering, Elsevier*, 51, pp.132-140.